

(ii) Dead and wind loads

● Windward side

$$\text{dead} + \text{wind} = 0.9 G_k + 1.4 W_k$$

$$\text{stress} = (0.9 \times 1.26)/1.4 - 1.4 \times 0.498 \quad (\text{from Table 12.3});$$

(proportionately reduced from above)

$$= 0.81 - 0.70 = 0.11 \text{ N/mm}^2 \quad (\text{no tension develops})$$

● Leeward side

$$\text{dead} + \text{wind} = 1.4 G_k + 1.4 W_k$$

$$\text{stress} = 1.26 + 1.4 \times 0.498 = 1.96 \text{ N/mm}^2$$

(iii) Dead, imposed and wind loads

$$\text{dead} + \text{imposed} + \text{wind} = 1.2 G_k + 1.2 Q_k + 1.2 W_k$$

$$\text{stress} = (1.26 \times 1.2)/1.4 + (0.13 \times 1.2)/1.6 \pm 1.2 \times 0.498$$

$$= 1.08 + 0.098 \pm 0.98$$

$$= 1.78 \text{ or } 0.58 \text{ N/mm}^2 \quad (\text{no tension develops})$$

The worst combination for this wall just above ground level also is dead+wind, and the design load is  $(1.96 \times 102.5 \times 10^3)/10^3 = 201 \text{ kN/m}$ .

#### 12.6.4 Selection of brick and mortar for inner leaf of wall B

The design vertical load resistance of the wall is  $(\beta f_k)/\gamma_m$  (clause 32.2.1). The value of  $\beta$  depends on the eccentricity of loading; hence the value of  $e$  needs to be evaluated before design can be completed.

#### 12.6.5 Calculation of eccentricity

The worst combination of loading for obtaining the value of  $e$  at top of the wall is shown in Fig. 12.6. Axial load

$$P = (0.9 \times 78.54 + 1.6 \times 7.29) \quad (G_k \text{ and } Q_k \text{ from Table 12.2})$$

$$= (70.69 + 11.66) = 82.35 \text{ kN/m}$$

First floor load

$$P_1 = (1.4 \times 6.48 + 1.6 \times 2.025) \quad (\text{see Table 12.2})$$

$$= 12.31 \text{ kN/m}$$

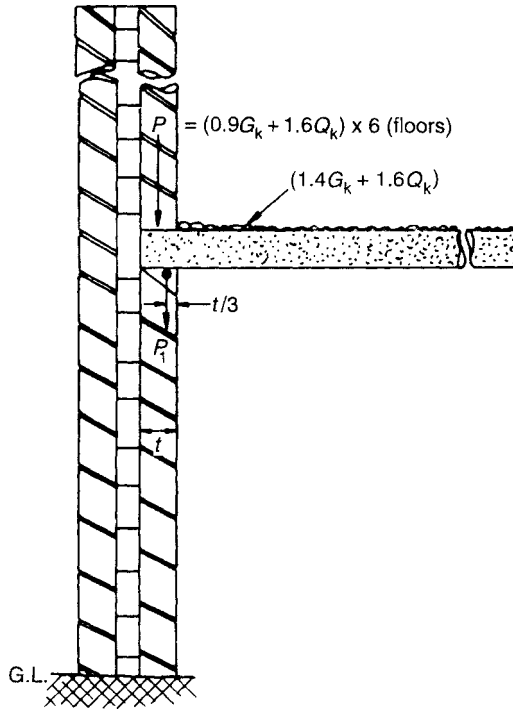


Fig. 12.6 Load combination for calculating the eccentricity.

Eccentricity

$$e = \frac{P_1 t}{6(P + P_1)} = \frac{12.31 t}{6(82.35 + 12.31)} = 0.0217t = 2.22 \text{ mm}$$

(a) Wind blowing north-south direction

A part of the panel B will be subjected to suction, if the wind is blowing in N-S direction. Then

$$V_s = VS_1 S_2 S_3 = 50 \times 1 \times 1 \times 0.64 \text{ (ground roughness category A, CP3,}$$

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$$= 32 \text{ m/s}$$

Note that the localized effect is considered here, hence  $S_2$  for Category A is being used. Also

$$q = 0.613 \times (32)^2 = 627.8 \text{ N/mm}^2$$